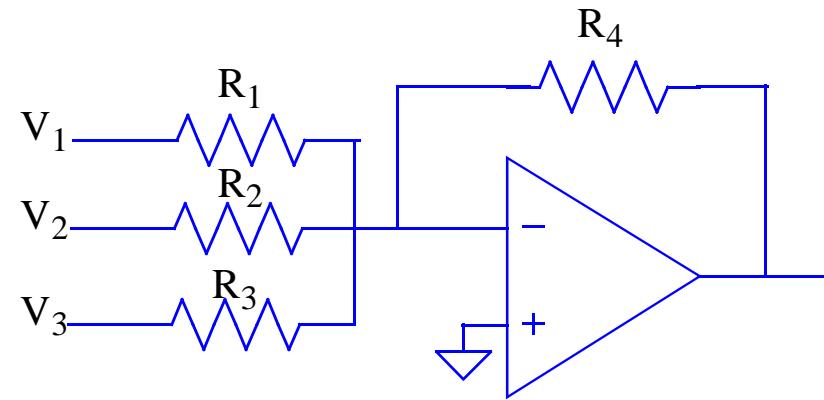


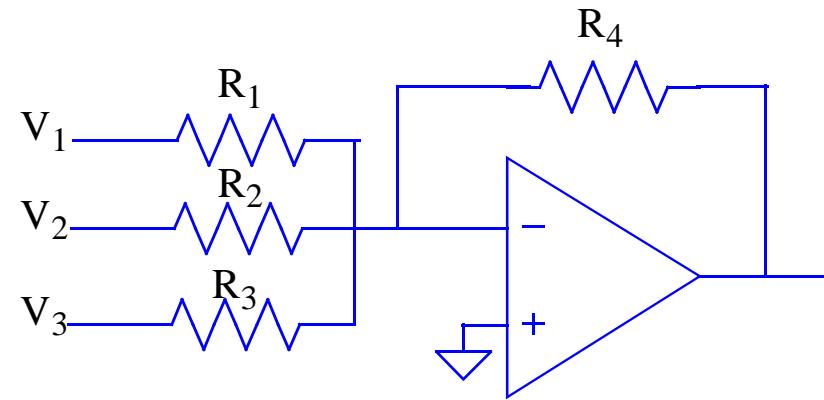
## Summing Amplifier Revisited

- Superposition can be used to easily evaluate summing amplifiers with infinite open loop gain



## Summing Amplifier Revisited

- Can we solve for the summing amplifier gain the same way when the open loop gain is finite?

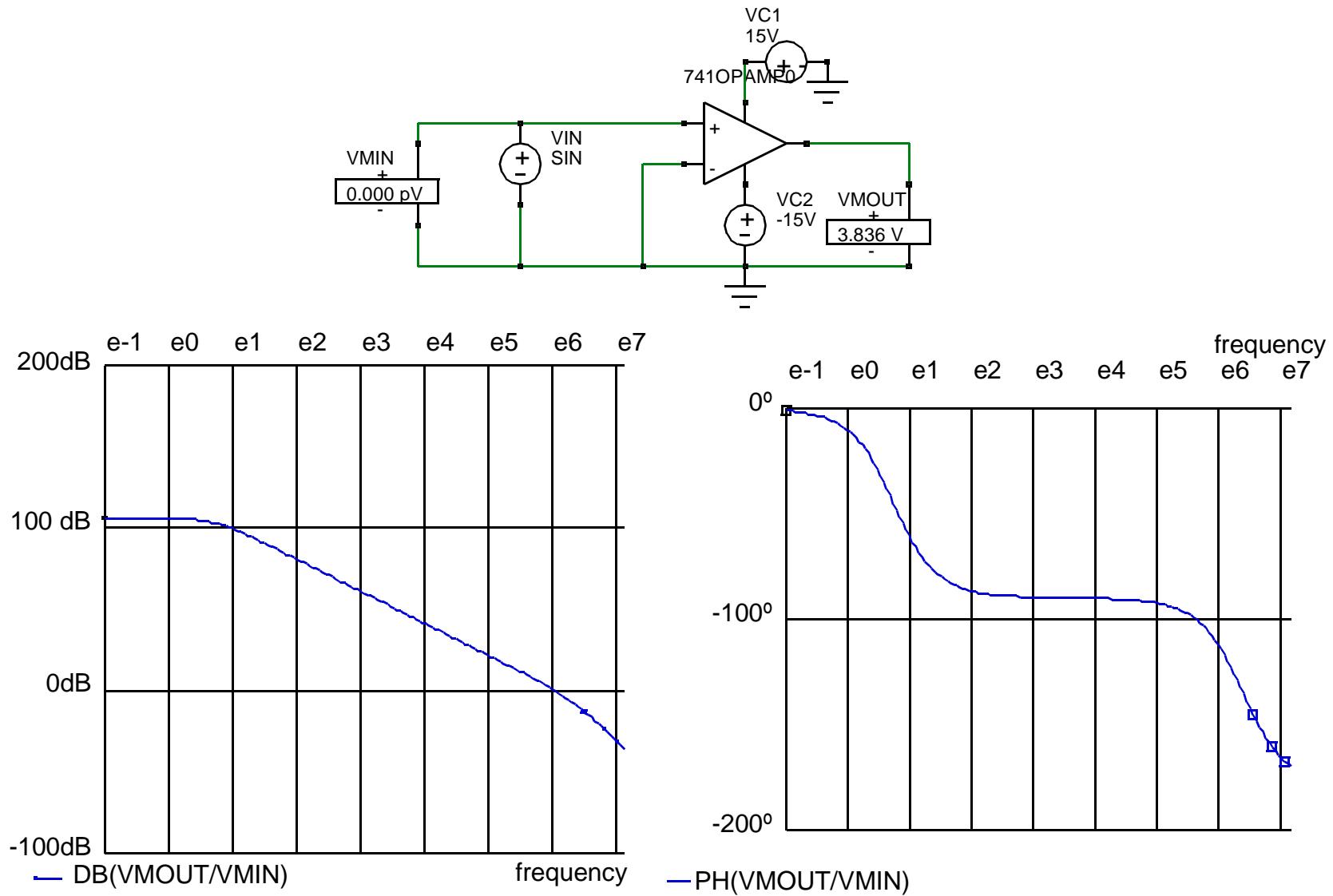


## Other Opamp Nonidealities

- The open loop gain is generally so large that we can neglect its impact on the closed-loop circuit gain
- But a significant nonideality that we cannot ignore is the finite open-loop gain as a function of frequency
- Parasitic capacitance causes the gain to fall off at high frequency (can't make  $\omega_H$  infinite for any amplifier!)
- The gain may be designed to change with frequency to ensure stability ---- compensation

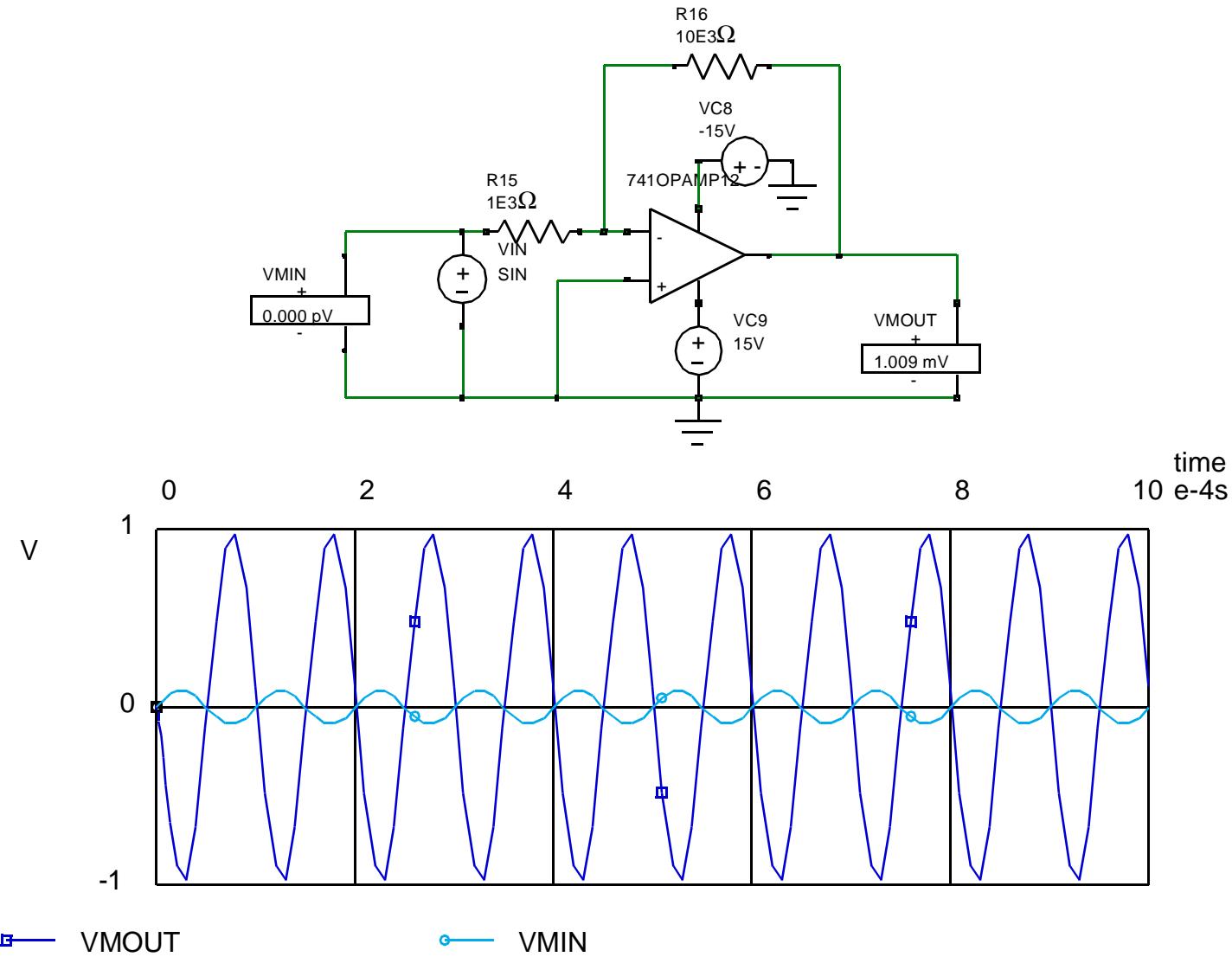
# 741 Opamp

- One of the most popular, general purpose opamps are the 741-type



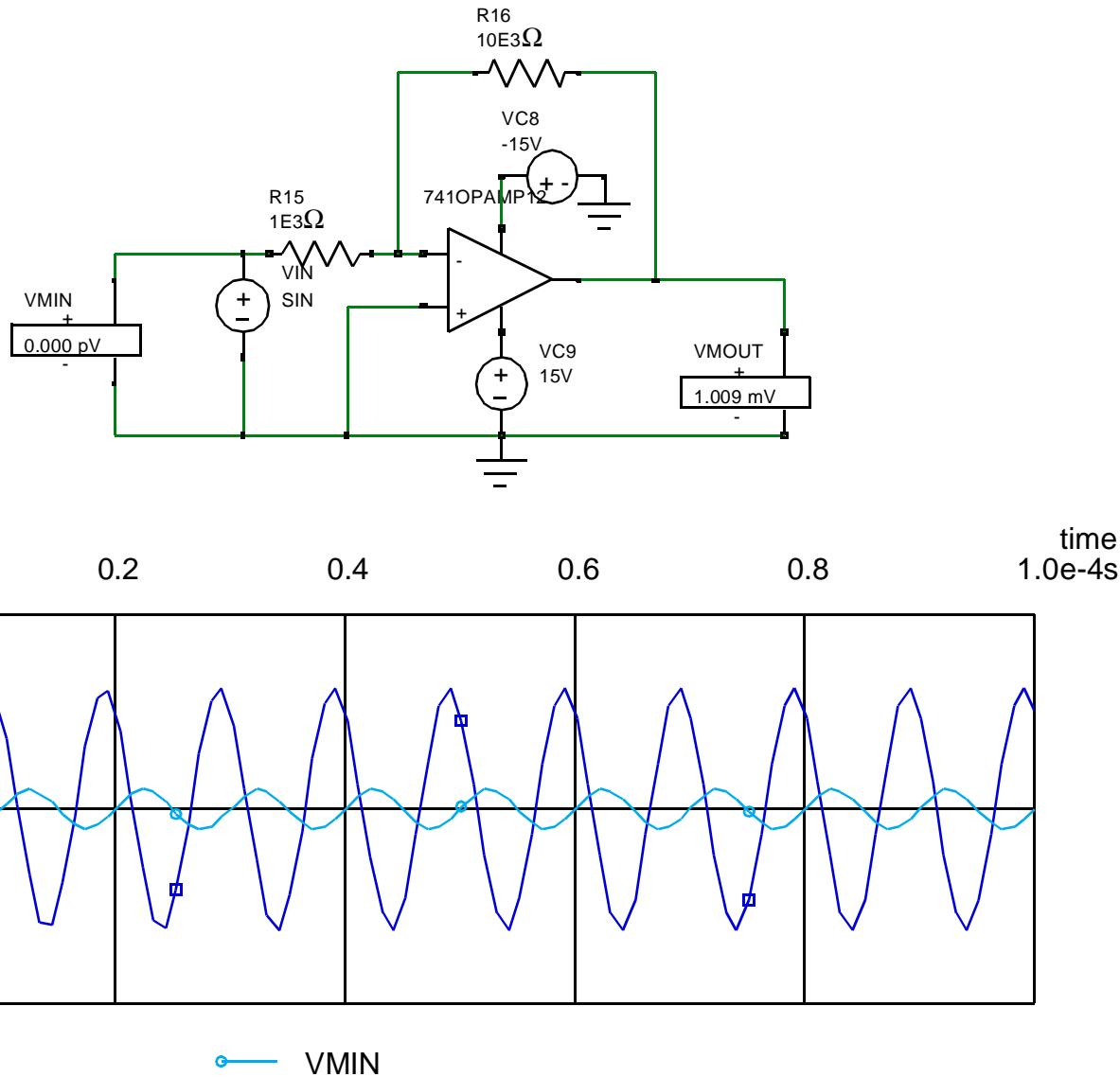
# 741 Opamp Example

- A gain of 10, or 20dB is possible at 10kHz:



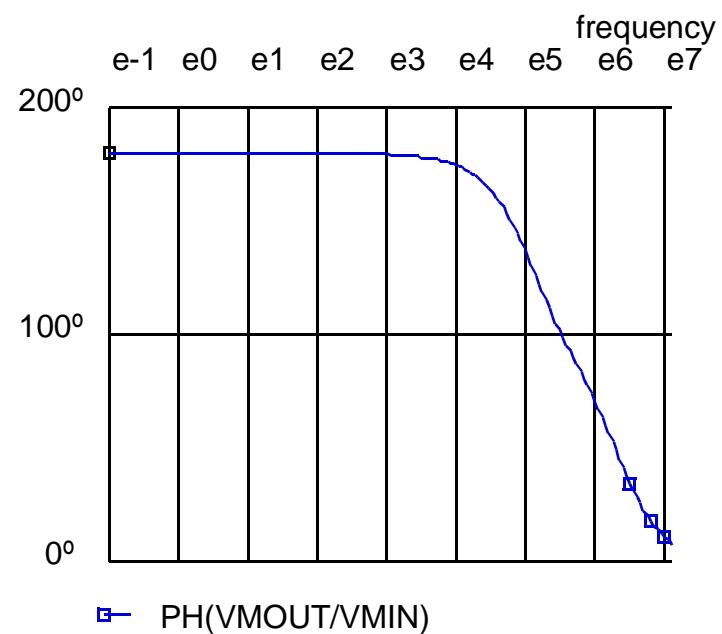
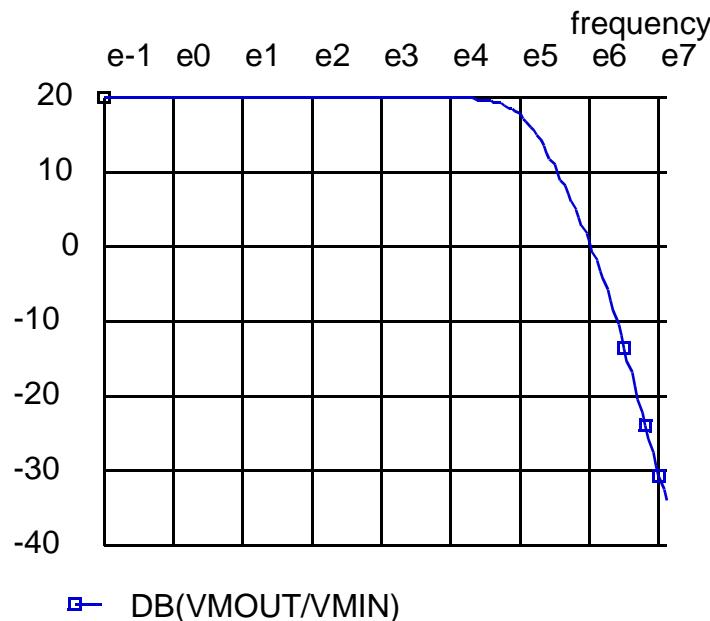
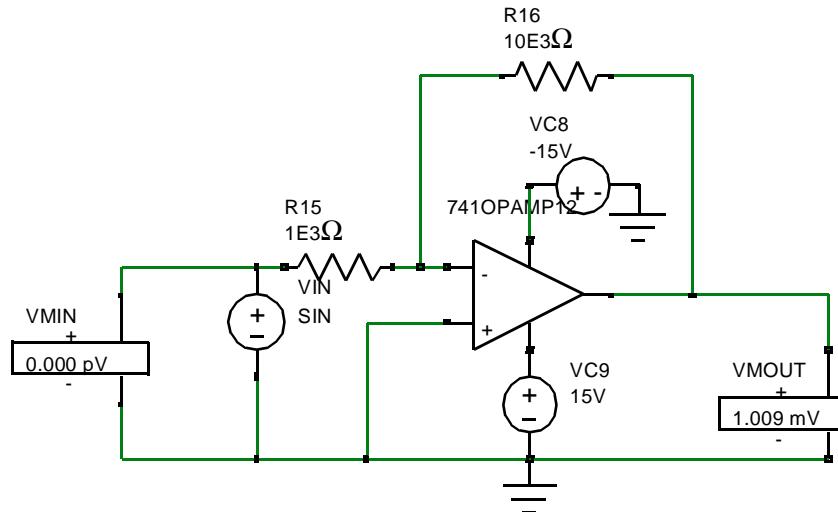
# 741 Opamp Example

- But not at 100kHz:



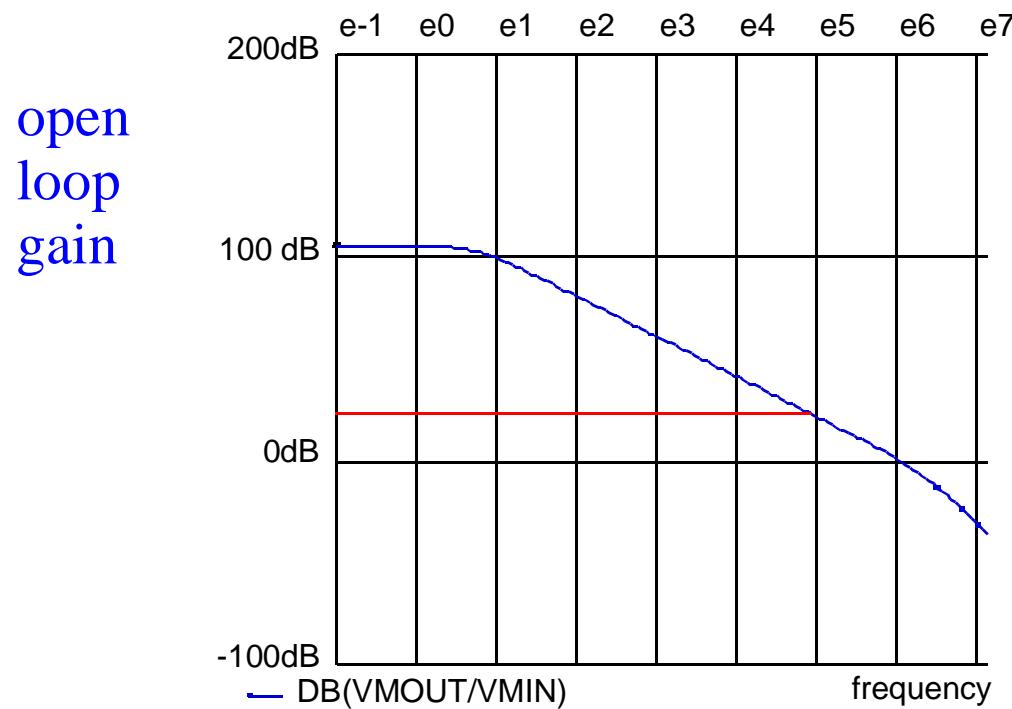
## 741 Opamp Example

- This decrease in gain is evident from a frequency domain analysis



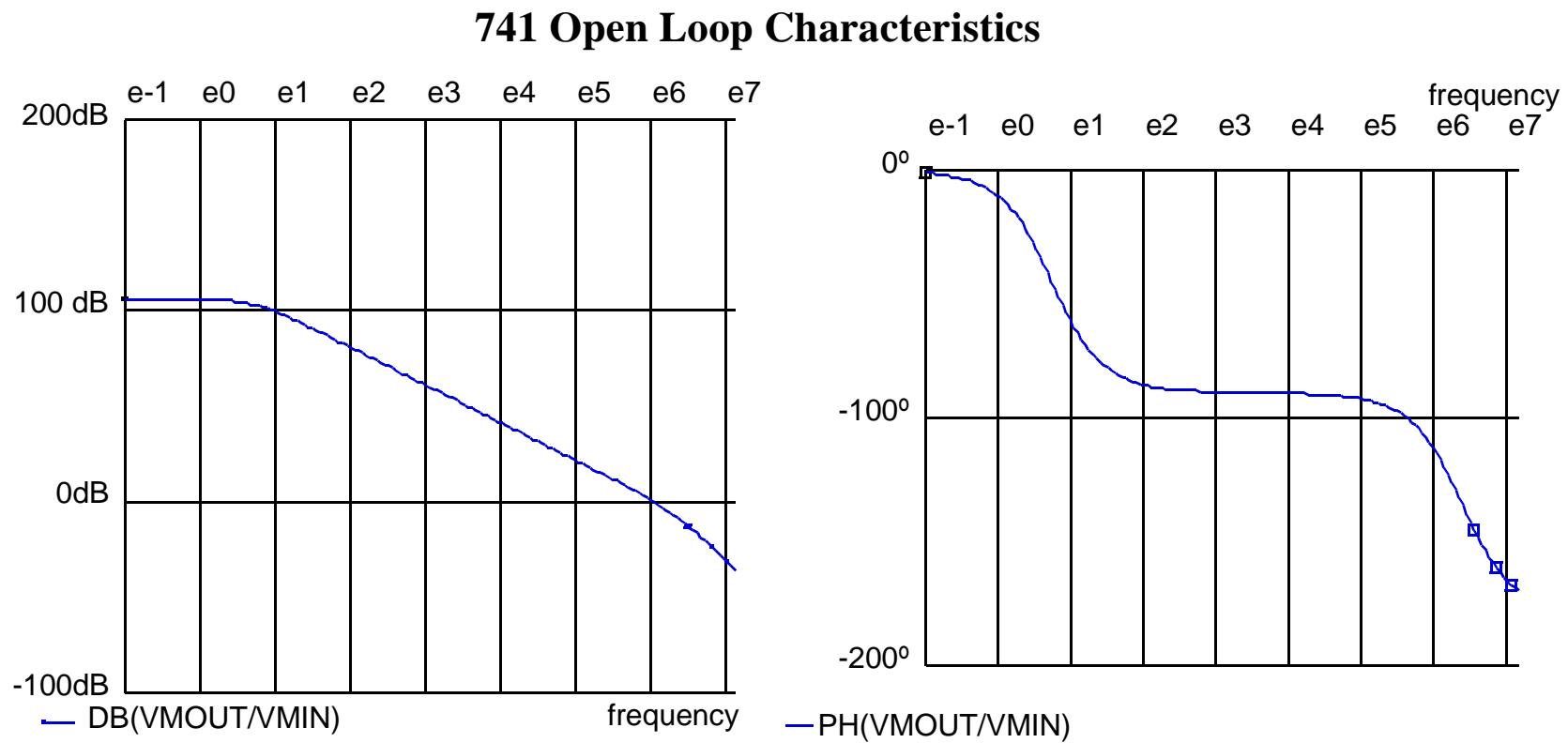
## Gain as a Function of Frequency

- Will the closed-loop gain (with feedback) will always be less than or equal to the open loop gain as a function of frequency?



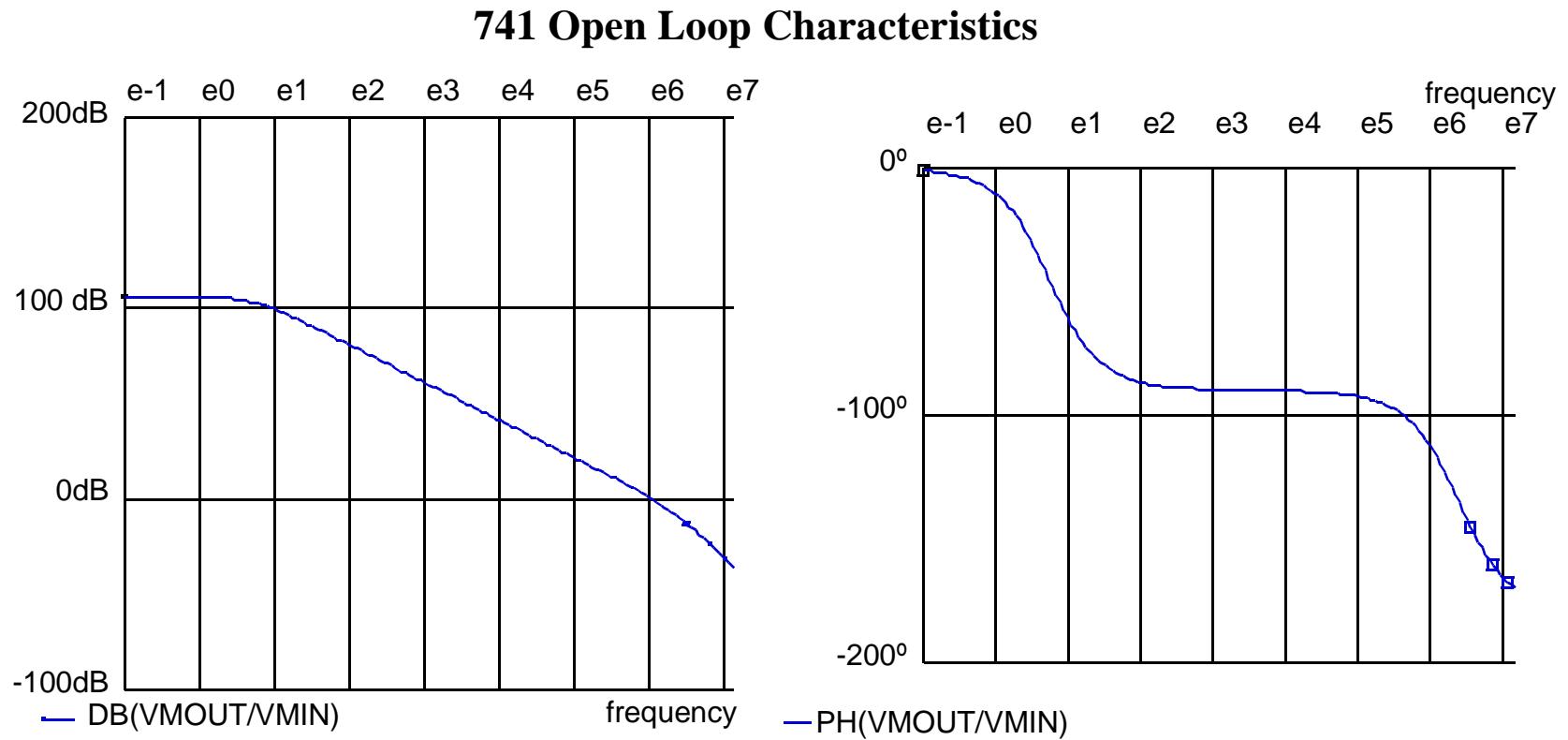
## Gain as a Function of Frequency

- We can assume that the close-loop response will follow the open loop characteristic beyond the frequency at which they intersect if the load capacitance and input terminal capacitances are small
- Why are the other capacitors a factor?



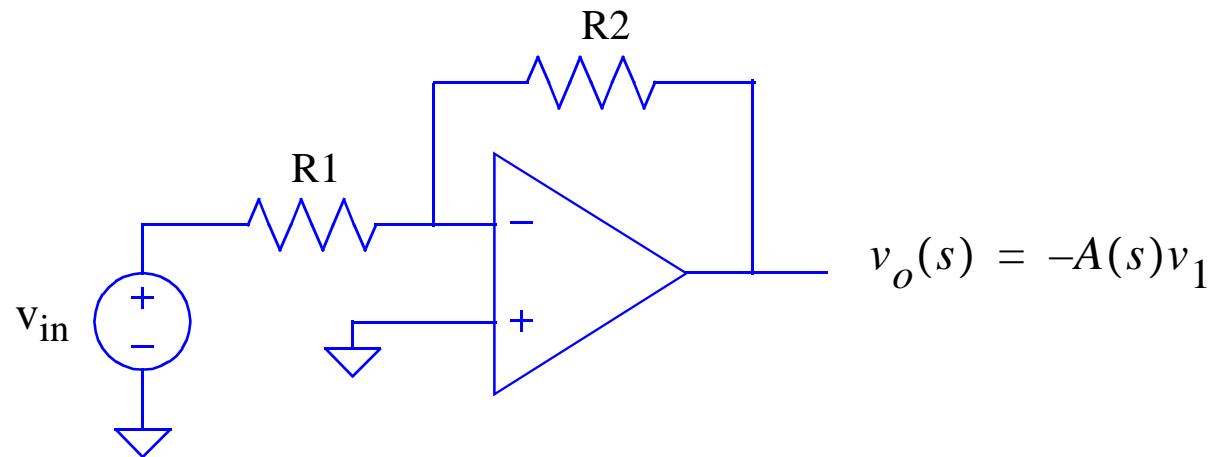
# Gain as a Function of Frequency

- It is important that the open loop characteristic has a phase shift of less than  $180^\circ$  (a change in gain of less than 40dB per decade) at the point of intersection with the closed-loop characteristic --- why?



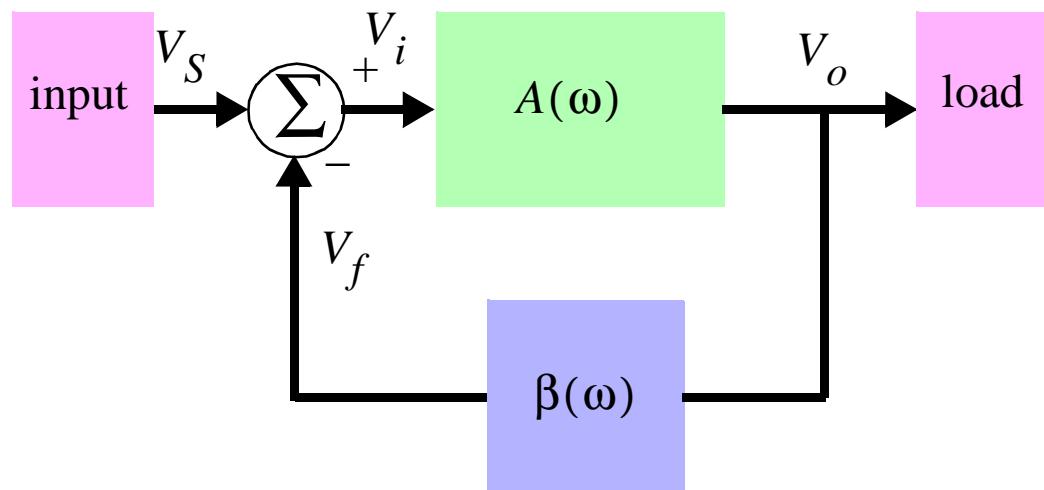
# Stability

- If the open loop gain has a phase shift of  $180^\circ$ , and we connect the opamp with negative feedback (which represents another phase shift of  $180^\circ$ ), then the total phase shift will be  $360^\circ$  which is like **positive feedback**



## Feedback

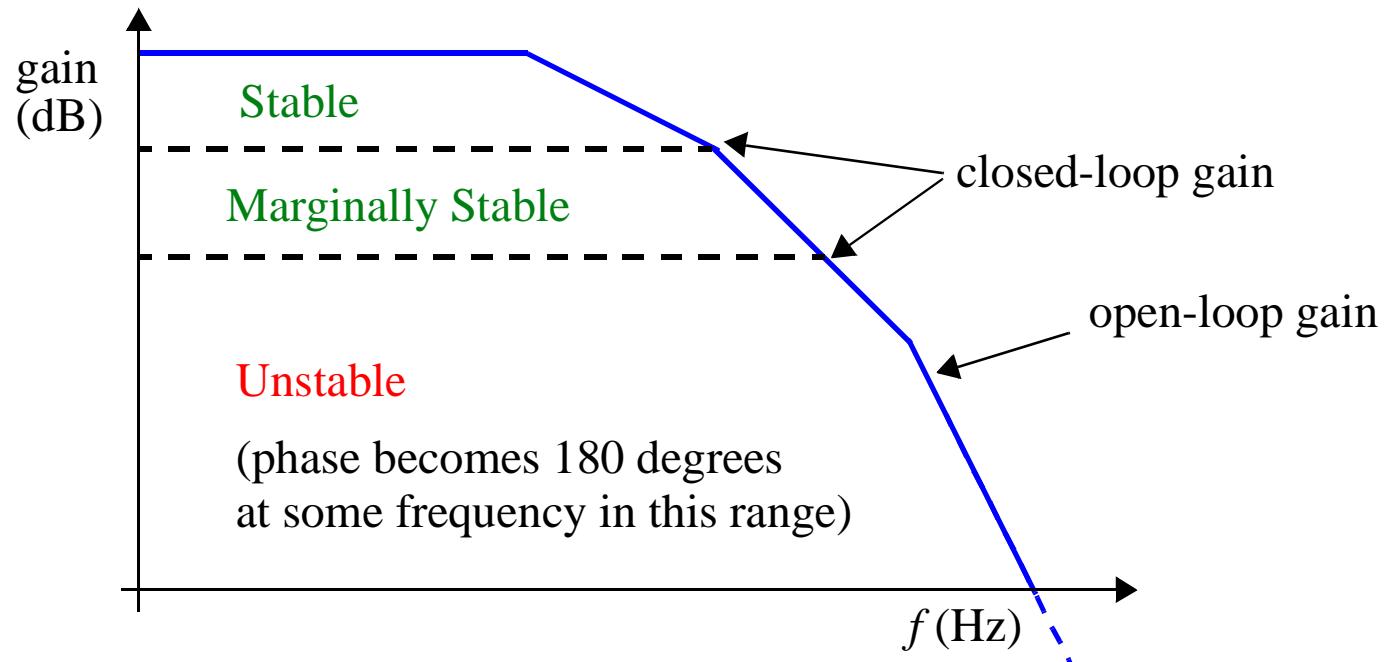
- The feedback can further complicate matters if it is also a function of frequency



$$A_f(\omega) = \frac{A(\omega)}{1 + \beta(\omega)A(\omega)}$$

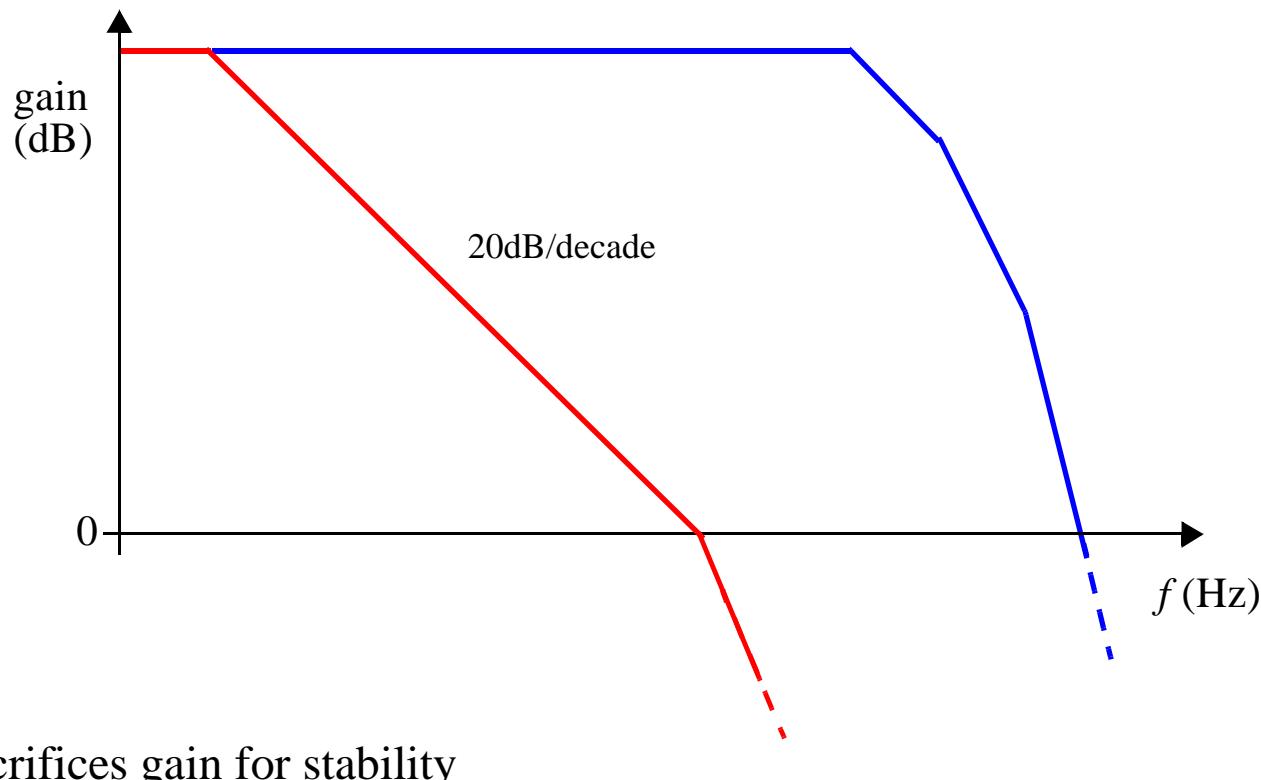
# Stability

- The circuit will be unstable with this positive feedback
- What causes the gain characteristic to exhibit these unwanted phase shifts?



## Internal Compensation

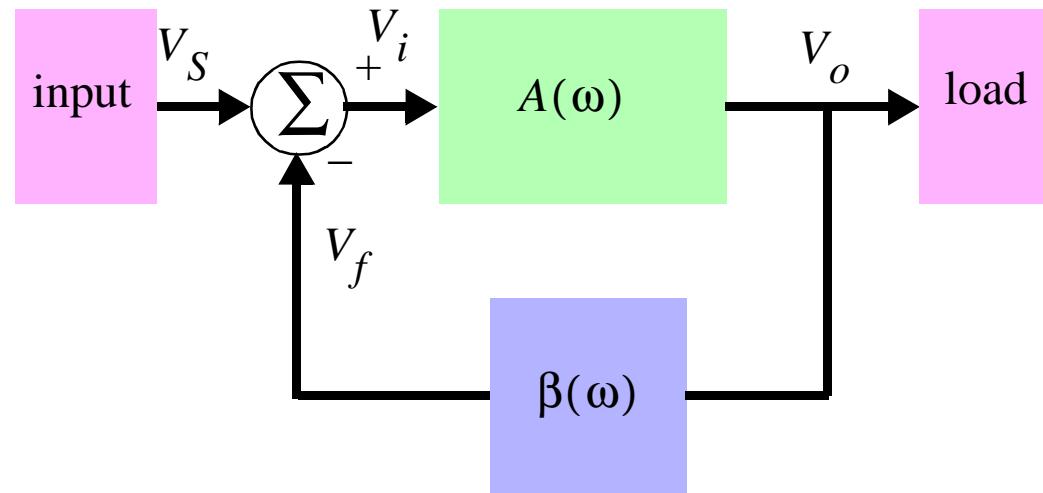
- Compensation capacitors are added to purposely place a low frequency (dominant) pole so that the change in gain will be 20dB/decade up until the unity gain frequency
- Why isn't the phase a concern beyond this frequency?



- Sacrifices gain for stability

## Feedback

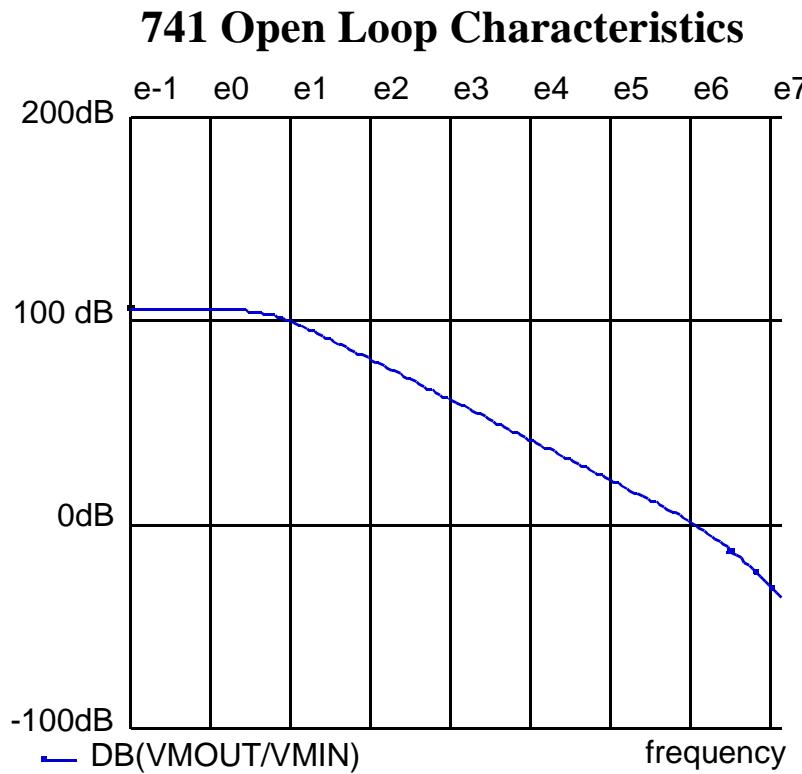
- Most feedback we've considered has no phase shift (resistors), so compensation will ensure stability
- However, frequency dependent feedback can pose a problem even for compensated opamps



$$A_f(\omega) = \frac{A(\omega)}{1 + \beta(\omega)A(\omega)}$$

## Modeling Gain as a Function of Frequency

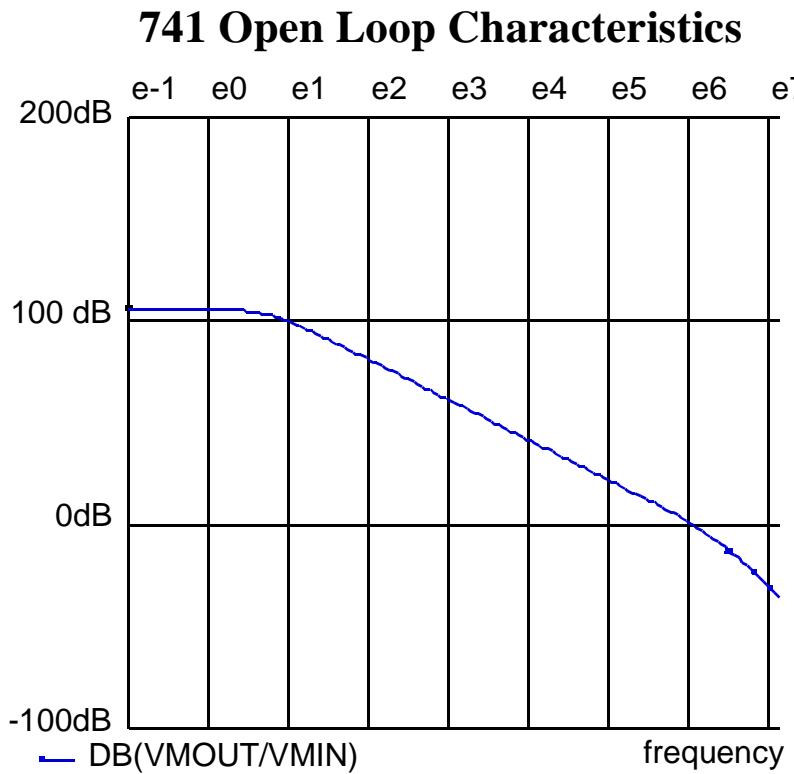
- With compensation, the frequency response appears like a STC



$$A(s) = \frac{A_o}{1 + s/\omega_b}$$

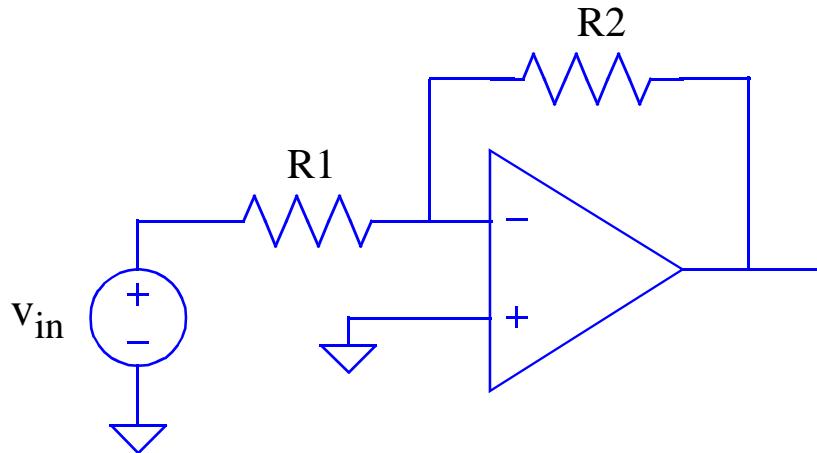
# Unity Gain Bandwidth

- We can easily solve for the frequency,  $\omega_t$ , at which the gain is 0dB



## Frequency Dependence of Gain

- Using these expressions for gain as a function of frequency we can approximate the inverting amplifier circuit gain as a function of frequency



$$\frac{V_o}{V_i} = \frac{-\frac{R_2}{R_1}}{1 + \frac{R_2}{R_1} A(s)}$$

$$A(s) = \frac{A_o}{1 + s/\omega_b}$$

$$\frac{V_o}{V_i} = \frac{-\frac{R_2}{R_1} A_o}{A_o + \left(1 + \frac{R_2}{R_1}\right) + \frac{s}{\omega_b} \left(1 + \frac{R_2}{R_1}\right)}$$

## Frequency Dependence of Gain

- We can assume that the closed-loop gain is much smaller than the dc open loop gain

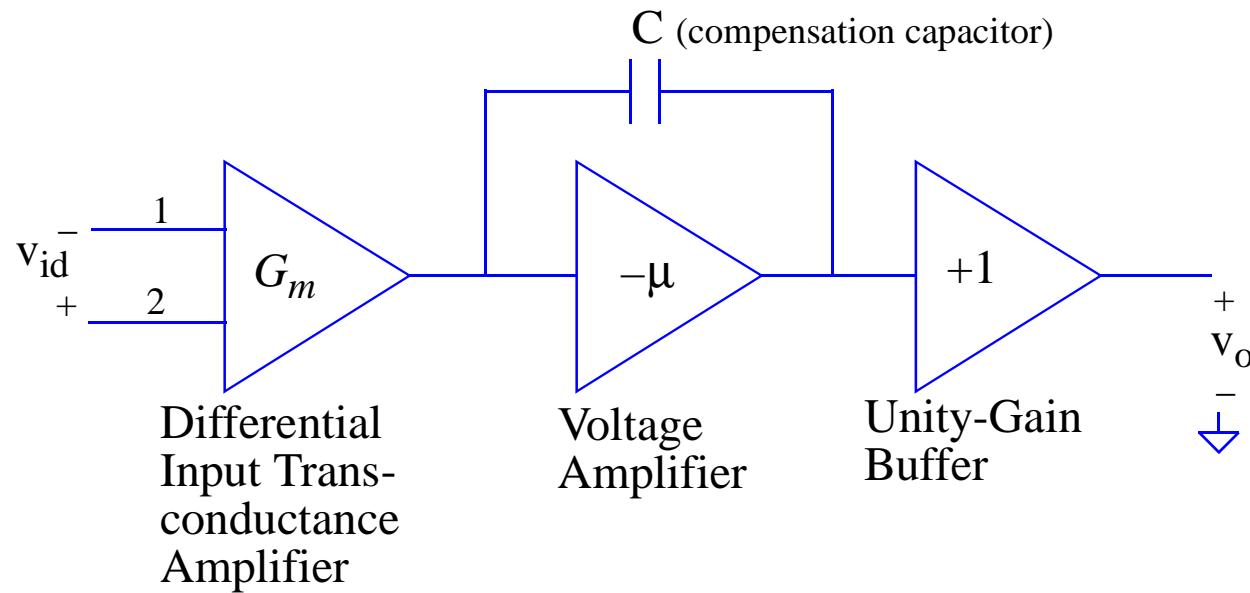
$$\frac{V_o}{V_i} = \frac{-\frac{R_2}{R_1}A_o}{A_o + \left(1 + \frac{R_2}{R_1}\right) + \frac{s}{\omega_b} \left(1 + \frac{R_2}{R_1}\right)}$$

## Frequency Dependence of Gain

- Does this result seem correct?

# Opamp Macromodels

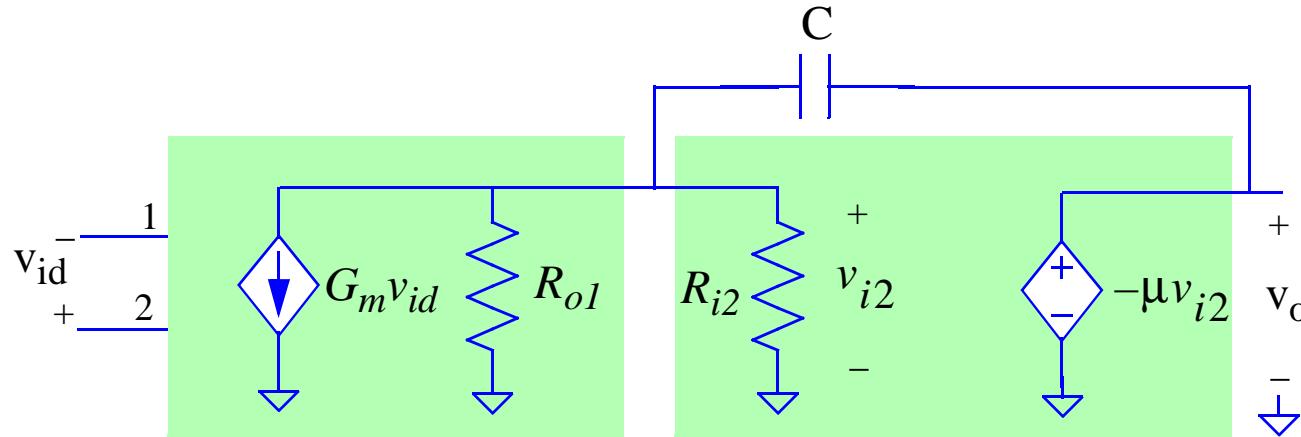
- We can model the frequency dependence of the gain using a macromodel for the opamp
- Internal structure of an opamp:



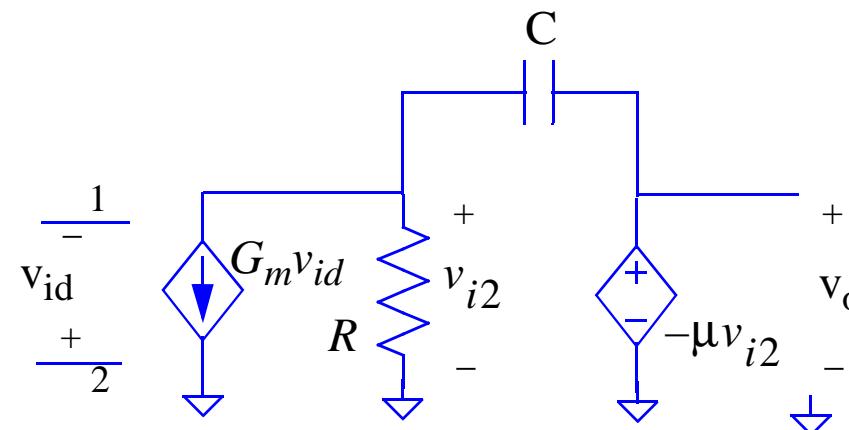
- We'll build all of these transistor level components later in the course

# Opamp Macromodels

- We can model the first two stages (the last is trivial) using controlled sources, R's and C's:

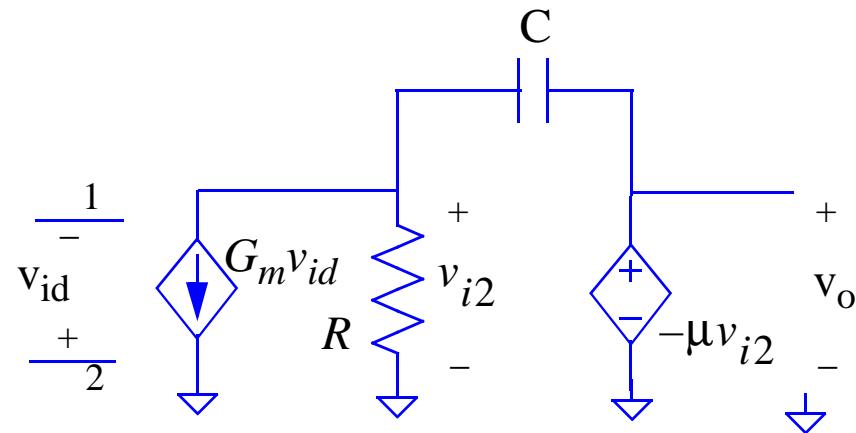


- Which we can simplify by combining the parallel R's

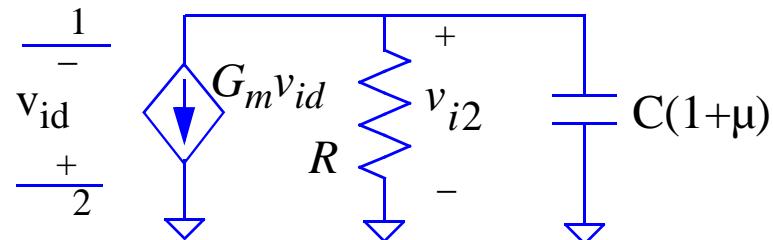


## Opamp Macromodel

- This circuit has the same STC form as a compensated opamp



# Opamp Macromodel



# Opamp Macromodel

- The parameters for a 741 macromodel are:

$$G_m = 0.19 \frac{mA}{volt} \quad \mu = 529 \quad R_{i2} = 4M\Omega \quad R_{o1} = 6.7M\Omega \quad C = 30pF$$

